A REVIEW ON SUPERCRITICAL WATER GASIFICATION OF BIOMASS

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Abstract - Supercritical water gasification is a promising and environmentally friendly biomass conversion method. Compared to conventional gasification, it is capable of handling biomass with high moisture and displays higher conversion efficiency and decreased tar formation. Through supercritical gasification, organic feedstock in the presence of supercritical water is converted into a mixture of H₂, CO₂, CO, CH₄ and traces of other gases over shorts periods of time. The composition and yield of the final gas mixture depends highly on reaction temperature, feed concentration and nature of catalyst in use. Reaction pressure and residence time play a less important role. Despite being appealing for the production of hydrogen from an inexpensive source, hydrothermal gasification suffers from decisive technical challenges, with corrosion and efficiency being the most critical.

Keywords: supercritical water gasification, SCWG, hydrothermal gasification, biomass, hydrogen

1. INTRODUCTION

Biomass poses as an attractive renewable energy source. It is practically abundant and does not participate in the increase of carbon dioxide in the atmosphere. However, the direct use of biomass as a fuel is challenging as it is a carrier of low energy density and possesses high moisture content. In addition, biomass displays heterogeneity, hydrophilic behavior and poor grindability. Conversion technologies that improve the physicochemical properties of the initial feedstock are necessary [1-3].

The conversion of biomass takes place through two main groups of processes: biochemical and thermochemical processes [4-5].

Biochemical processes convert biomass into energy primarily through fermentation and anaerobic digestion. Fermentation leads to the production of bioethanol through the use of microorganisms and enzymes, while anaerobic digestion employs bacterial activity in an anaerobic environment for the production of biogas [4-6].

Thermochemical processes use heat under the presence of a catalyst. The main thermochemical pathways are combustion, liquefaction, gasification and

pyrolysis [4, 6]. The direct combustion of biomass is the most technologically mature method even though it requires feedstock with low moisture and is characterized by low efficiency [4-5, 7]. Pyrolysis takes place under elevated temperatures (between 500-1000 °C) in an oxygen-deprived environment and leads to the production of bio-oil (bio-crude), a liquid fraction with high heating value, biochar, a solid carbon-rich residue suitable for soil amendment, and a mixture of noncondensable gases [5, 8-9]. In hydrothermal liquefaction, commonly known as liquefaction, biomass is being converted into bio-oil in the presence of both a solvent and a catalyst and at temperatures between 200-400 °C [10-13]. Gasification involves the partial oxidization of biomass at high temperatures (700-1500 °C) within a gasification medium (air, steam or oxygen). The main product is a mixture of hydrogen, carbon monoxide, carbon dioxide, methane, and other gases in smaller quantities [4, 14-16]. In Fig. 1, the main thermochemical routes of biomass conversion are depicted.

Thermochemical processes, when compared to biochemical, display specific advantages. While biochemical methods are biomass-specific, thermochemical are capable of using a wider variety of biomass types. Their duration spans from a few minutes to several hours, when biochemical require several days. Finally, thermochemical processes are characterized by higher conversion efficiency [4, 6, 9].

Most thermochemical processes are dry conversion processes, meaning that they can work efficiently only with organic feedstock that has low moisture content. Hydrothermal carbonization, liquefaction and gasification are capable of handling organic feedstock with high moisture content since the presence of water is required. Thus, the initial energy-intensive drying step is rendered redundant. In addition, the conditions (reaction temperature and pressure) affect the properties of water in ways that are beneficial to the degradation of biomass and its subsequent reformation into the final products [18-20]. In Fig. 2, the classification of hydrothermal processes as a function of reaction temperature and pressure is shown.

The focus of this paper is the process of supercritical water gasification. SCWG is a specific type of hydrothermal gasification that takes place under supercritical water conditions and leads to the production of hydrogen. Compared to its dry counterpart, it requires

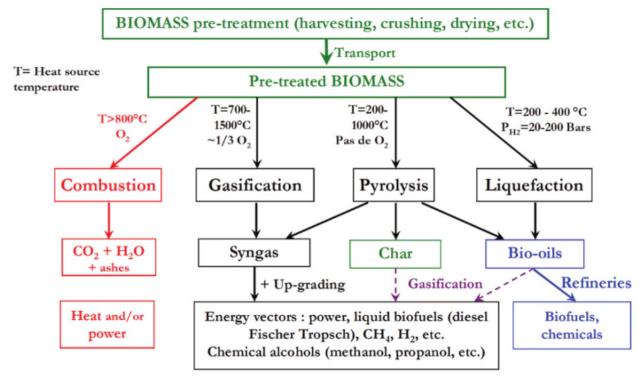
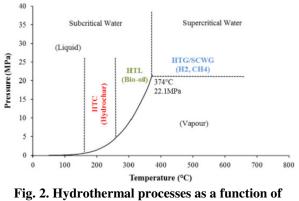


Fig. 1. Main thermochemical routes for biomass conversion [17].

lower reaction temperatures, leads to lower tar formation, and, depending on the process parameters, may display relatively high conversion rates. Furthermore, hydrogen as a fuel is environmentally clean since its combustion releases water [19, 21-28].



temperature and pressure [9].

2. SUPERCRITICAL WATER GASIFICATION

Gasification is a thermochemical conversion that produces a combustible mixture of gases (mainly H_2 , CO, CO₂ and CH₄) through the partial oxidization of solid organic feedstock. It takes place under high temperature (700-1500 °C) and pressure (20-30 MPa) and in the presence of a gasification agent such as air, steam or oxygen [14, 28]. Hydrothermal gasification is a variation that involves lower temperatures and the use of water as a reaction medium. The aqueous environment makes the process ideal for the conversion of wet biomass with high moisture content [14, 21]. Hydrothermal gasification can be classified into three categories: catalyzed aqueousphase reforming (215-265 °C) for the production of hydrogen, catalyzed gasification (350-400 °C) for the production of methane, and supercritical water gasification (600-700 °C) for the production of hydrogen [18-23].

Supercritical water gasification (SCWG), which is the focus of this paper, displays specific advantages over conventional gasification. As a hydrothermal process, it takes place in the presence of water under high temperature and pressure (higher than 374 °C and 22.1 MPa). High pressure is necessary in order to suppress the evaporation of water into steam. The use of water as a reaction medium makes the process ideal for handling organic feedstock with high moisture content and at the same time renders the preliminary energy-intensive drying step of conventional gasification processes redundant. Furthermore, water is capable of dissolving intermediate products, thus reducing the formation of tar and solid byproducts. Under supercritical conditions, water acts both as a reaction medium and as a reactant. Its properties (density, dielectric constant, ion product) are beneficial to the degradation of organic compounds [14-16, 17-37].

Supercritical water gasification mainly involves the following three reactions: steam reforming (1), water-gas shift (2) and methanation reactions (3).

$$Biomass + H_2O \to H_2 + CO \tag{1}$$

$$CO + H_2O \leftrightarrow CO_2 + H_2$$
 (2)

$$CO + 3H_2 \leftrightarrow CH_4 + H_2O$$
 (3)

The two-way arrow suggests that the respective reactions are in equilibrium and, depending on the process parameters, may proceed either way [21, 33]. In steam reforming, supercritical water reacts with organic feedstock producing hydrogen and carbon monoxide. The carbon monoxide reacts, in turn, with water producing hydrogen and carbon dioxide via water-gas shift reaction. In methanation reaction, carbon monoxide from steam reforming and hydrogen from water-gas shift react producing methane and water [15, 28-29, 36].

The conventional gasification technologies consist mainly of fixed bed, fluidized bed and entrained bed gasifiers.

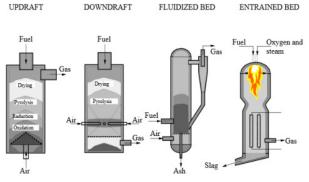


Fig. 3. Conventional gasification technologies: fixed bed (updraft and downdraft), fluidized bed and entrained bed [22].

Fixed bed gasifiers are further classified into updraft and downdraft, depending on the direction of the airflow. In an updraft fixed bed gasifier the fuel inlet and gas outlet reside at the top while the inlet of the gasifying agent resides at the bottom. The rising gasifying agent comes in contact with hot unconverted biomass charcoal and hot CO_2 and H_2O are produced, which in turn react endothermically with char and form CO and H_2 . Even thought updraft gasifiers have very high conversion efficiencies (up to 80%), the produced gases contain high amounts of tar.

Downdraft gasifiers display lower efficiency since the gases exit at high temperatures (900-1000 $^{\circ}$ C). In downdraft gasifiers, the biomass feed and the air are moving in the same direction even though air enters the reactor at a lower part of the gasifier through radially directed nozzles. The fact that the gases pass through the hot zone before exiting, enables the partial cracking of formed tar leading to lower tar content. Downdraft gasifiers, when compared to updraft display lower efficiency since the gases exit with high temperature. On the other hand, the final product contains less amount of tar and ash.

In the case of fluidized bed gasifiers, the air is moving upwards through a biomass bed playing the role of the fluidizing gas. This provides temperature uniformity since air and solid phase come in excellent thermal contact. Fluidized bed gasifiers employ temperatures between 800-1000 °C in order to avoid the accumulation of ash. Despite its flexibility in terms of feed rate and consumption rate, these gasifiers produce more ash and tar compared to downdraft gasifiers.

Entrained bed gasifiers encounter problems processing fibrous materials and therefore are unsuitable for many types of biomass and applications [14-16, 18-19, 22, 37].

3. PROCESS PARAMETERS

Reaction temperature and pressure, biomass concentration, residence time and the use of catalysts have been recognized as the most influential process parameters [28].

Temperature is considered to be the dominant parameter that affects gasification efficiency and product quality. Higher temperatures favor H₂ and CO₂ formation, while lower temperatures are associated with increased CH₄ and CO yields [28]. This is attributed to the underlying reaction mechanism. At lower gasification temperatures, the endothermic methanation reactions are prevalent, while at higher temperatures the exothermic reforming and water-gas shifting reactions are being promoted (Le Chatelier principle or equilibrium law). This is why temperatures up to 400 °C favor methane production, while higher temperatures up to 600 °C or greater lead to increased hydrogen yields [18, 35]. At higher temperatures, SCWG achieves higher product yield at the cost of energy efficiency. The use of catalysts can effectively lower the gasification temperature [18, 35]. Reaction temperature also affects the production of CO and CO_2 in a similar fashion. As temperature increases, CO₂ production increases at the expense of CO [24, 28].

It has been found that by increasing pressure the gas composition shifts in favor of methane. The effect of reaction pressure, however, was found to be negligible in comparison with reaction temperature [24, 35].

Feed concentration has an adverse effect on gasification efficiency. Apart from being associated with pumping and plugging issues, high feedstock concentrations are linked with reduced hydrogen and increased methane yields. This is attributed to the amount of water required for the formation of each product. H₂ requires much more water than CH₄. An example of the effect of temperature and feed concentration on the gas yields is depicted in Fig. 4. The hydrogen and methane yields of wood sawdust gasification are evidently antagonizing [24, 28, 35].

Biomass decomposition generally occurs rapidly in SCWG. Residence time also affects the product yield but to a much lesser extent. Initially, prolonged retention times lead to increased gas production. However, after a certain point, the effect of duration is marginal. Whether prolonged times will benefit methane or hydrogen yield depends on the feedstock in use [19, 21, 27].

SCWG takes place under high temperature and pressure. The use of specific catalysts such as alkali, transition metals and activated carbon that improve the process has been investigated. The presence of a catalyst lowers the required extreme operating conditions, thus improving the efficiency of the process. In addition, catalysts are connected with improved H_2 yields (high hydrogen production selectivity) and the suppression of tar and char formation [18, 28].

Homogeneous catalysts such as alkali metals $(Na_2CO_3, KHCO_3, K_2CO_3, NaOH etc.)$ are often used to improve the water-gas shift reaction. Such catalysts, however, are dissolved in the supercritical water, making it difficult to recover. They are also associated with reactor fouling, plugging and corrosion. Heterogeneous

catalysts consist of transition metals (Ni, Ru, Rh, Pt etc), activated carbons and oxides (oxides of Cu, Mn, Co, Al

and others). These catalysts usually enhance methanation and steam reforming reactions. In addition, they display

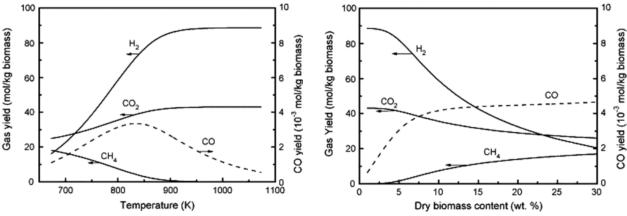


Fig. 4. Gas yields as a function of temperature and dry biomass content of wood sawdust gasification [24].

higher hydrogen selectivity and catalytic activity. Heterogeneous catalysts are considered superior to their homogeneous counterparts due to their increased recyclability. Among the typical SCWG catalysts are KOH, KHCO₃, Na₂CO₃ and the noble metals Ru, Rh and Pt [18, 23, 28-29, 35].

4. TECHNICAL CHALLENGES

Supercritical water gasification is considered to be a promising biomass conversion method. However, its commercial application faces several challenges.

SCWG is a relatively expensive application and therefore is suitable for the conversion of biomass with high disposal cost. Due to the high cost of installation and operation, the integration of SCWG with other processes for power generation and CO_2 capture has been speculated [21, 31]. Compared to other conventional methods for the production of hydrogen, supercritical water gasification is the most cost effective process. Compared to fossil fuels, the cost of hydrogen produced by renewable energy sources is still very high [36].

SCWG is often associated with plugging and corrosion of the reactor [21]. This is attributed to the extreme operating conditions and to unwanted intermediate products that are formed during the process. SCWG reactors require materials that are able to withstand these adverse conditions of temperature and pressure as well as the corrosion. Nikel-based alloys as reactor construction materials is a common solution. Another promising alternative which is currently under investigation is the use of ceramic materials such as aluminum oxide (alumina, Al₂O₃). Novel circulating flow reactor designs that prohibit the contact of corrosive materials with solid surfaces have also been proposed. Apart from increasing the selectivity to hydrogen and suppressing the formation of tar, the use of catalysts may be employed for the efficient reduction of the required reaction temperature and pressure [18, 28, 33-34]. A research effort has been made towards the development of tubular reactor that deals with plugging. These reactors are prone to intermittent function due to the formation of char and ash build-up. It has been

speculated that high reaction temperature and high heating rate at the entrance of the reactor may be beneficial to the plugging of the reactor [28, 30].

Even though supercritical water gasification doest not require a preliminary feedstock drying, whose energy is irrecoverable, it still suffers from thermal efficiency issues. Fortunately, despite the high temperature requirement, a significant amount of sensible heat can be recovered from the exiting gaseous mixture using a high efficiency heat exchanger. This would increase the overall performance of the process [14, 28, 31, 35].

Finally, the feedstock composition may be of importance. Experiments have shown that lignin content has a negative effect on hydrogen production. Intermediate products react with lignin, thus reducing the potential hydrogen yield [24].

5. CONCLUSIONS

Supercritical water gasification is a biomass conversion method that stands out. It is capable of converting organic feedstock with high moisture content into hydrogen and other gases with high yields over short times. High operating pressures allow less energy consumption for gas storage and smaller reactor dimensions and consequent heat losses. Feedstock and reaction medium are inexpensive. Its final product is superior than that of conventional dry gasification.

However, the application of SCWG at an industrial level faces important techno-economical obstacles. This conversion method is relatively new and a limited amount of applications exist outside a laboratory. Frequent maintenance and product purification are adding to the pre-existing installation complexity and high operating costs. The severe operating conditions and the issues of reactor corrosion and plugging are a challenge for the designing and manufacturing of gasification reactors. Understanding the underlying reaction mechanism combined with newer reactor designs and experimentation on catalysts will hopefully lead towards a more efficient hydrogen production [18, 20, 31-32, 34-35].

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REFERENCES

- [1]. P. McKendry. Energy production from biomass (part 1): overview of biomass. Bioresource Technology 83 (2002) 37-46.
- [2]. E. Sermyagina et al. Hydrothermal carbonization of coniferous biomass: Effect of process parameters on mass and energy yields. Journal of Analytical and Applied Pyrolysis 113 (2015) 551-556.
- [3]. B. Erlach et al. Co-production of electricity, heat and biocoal pellets from biomass: a techno-economic comparison with wood pelletizing. World Renewable Energy Congress 2011-Sweden, 8-13 May 2011, Linkoping Sweden
- [4]. A. Kumar et al. Thermochemical biomass gasification: A review of the current status of technology. Energies 2009, 2, 556-581; doi: 10.3390/en20300556
- [5]. P. McKendry. Energy production from biomass (part 2): conversion technology. Bioresource Technology 83 (2002) 47-54.
- [6]. R. Mehrabian et al. Application of numerical modelling to biomass grate furnaces. Journal of Thermal Engineering, Yildiz Technical University Press, Istanbul, Turkey, Vol. 1, Special Issue 3, No. 6, pp. 550-556, May, 2015.
- [7]. C. T. Primaz et al. Influence of the temperature in the yield and composition of the bio-oil from the pyrolysis of spent coffee grounds: Characterization by comprehensive two dimensional gas chromatography. Fuel 232 (2018) 572-580.
- [8]. H. S. Kambo, A. Dutta. A comparative review of biochar and hydrochar in terms of production, physico-chemical properties and applications. Renewable and Sustainable Energy Reviews 45 (2015) 359-378.
- [9]. W. Jiang et al. Liquefaction of lignocellulosic materials and its applications in wood adhesives-A review. Industrial Crops & Products 124 (2018) 325-342.
- [10].S. S. Toor et al. Hydrothermal liquefaction of biomass: A review of subcritical water technologies. Energy 36 (2011) 2328-2342.
- [11].A. Dimitriadis, S. Bezergianni. Hydrothermal liquefaction of various biomass and waste feedstocks for biocrude production: A state of the art review. Renewable and Sustainable Energy Reviews 68 (2017) 113-125.
- [12].M. Magdelin et al. Techno-economic assessment of integrated hydrothermal liquefaction and combined heat and power production from lignocellulose residues. J. sustain. Dev. Energy water environ. Syst., 6(1), pp 89-113, 2018, DOI: https://doi.org/10.13044/j.sdewes.d5.0177
- [13].B. Zhou et al. Tar formation and evolution during biomass gasification: An experimental and theoretical study. Fuel 234 (2018) 944-953.
- [14].P. McKendry. Energy production from biomass (part 3): gasification technologies. Bioresource Technology 83 (2002) 55-63.
- [15].A. Uzi. Permittivity and chemical characterization of woody biomass during pyrolysis and gasification. Chemical Engineering Journal 355 (2019) 255-268.
- [16].A. Dufour. Thermochemical conversion of biomass for the production of energy and chemicals.2016, New Jersey, John Wiley & Sons.

- [17].M. Kumar et al. A review on the current status of various hydrothermal technologies on biomass feedstock. Renewable and Sustainable Energy Reviews 81 (2018) 1742-1770.
- [18].R. Singh et al. Strategies for selection of thermo-chemical processes for the valorisation of biomass. Renewable Energy 98 (2016) 226-237.
- [19].B. Patel et al. A review on hydrothermal pre-treatment technologies and environmental profiles of algal biomass processing. Bioresource Technology 199 (2016) 288-299.
- [20].A. Kruse et al. Hydrothermal conversion of biomass to fuels and energetic materials. Current opinion in Chemical Biology 2013, 17: 515-521.
- [21].C. R. Correa, A. Kruse. Supercritical water gasification of biomass for hydrogen production-Review. The Journal of Supercritical Fluids 133 (2018) 573-590.
- [22].S. Farzad et al. A critical review on biomass gasification, co-gasification, and their environmental assessments. Biofuel Research Journal 12 (2016) 483-495.
- [23].Y. Guo et al. Review of catalytic supercritical water gasification for hydrogen production from biomass. Renewable and Sustainable Energy Reviews 14 (2010) 334-343.
- [24].A. Kruse. Supercritical water gasification. Biofuels, Bioprod. Bioref. 2:415-437 (2008).
- [25].A. Kruse. Hydrothermal biomass gasification. J. of Sustainable Fluids 47 (2009) 391-399.
- [26].P. T. Williams, J. Onwudili. Composition of products from the supercritical water gasification of glucose: a model biomass compound. Ind. Eng. Chem. Res. 2005, 44, 8739-8749.
- [27].S. N. Reddy et al. Supercritical water gasification of biomass for hydrogen production. International Journal of Hydrogen Energy 39 (2014) 6912-6926.
- [28].S. Reddy et al. Supercritical water gasification of biomass for hydrogen production. International Journal of Hydrogen Production 39 (2014) 6912-6926.
- [29].L. Qian et al. Treatment of municipal sewage sludge in supercritical water: A review. Water Research 89 (2016) 118-131.
- [30].Y. J. Lu et al. Hydrogen production by biomass gasification in supercritical water: A parametric study. International Journal of Hydrogen Energy 31 (2006) 822-831.
- [31].Z. Chen et al. A power generation system with integrated supercritical water gasification of coal and CO₂ capture. Energy 142 (2018) 723-730.
- [32].D. Lachos-Perez et al. Supercritical water gasification of biomass for hydrogen production: Variable of the process. Food and Public Health 2015, 5 (3): 92-101. DOI: 10.5923/j.fph.20150503.05.
- [33].O. Yakaboylu et al. Supercritical water gasification of biomass: a literature and technology overview. Energies 2015, 8, 859-894; doi: 10.3390/en8020259.
- [34].D. Castello et al. Supercritical water gasification of biomass in a ceramic reactor: long-time batch experiments. Energies 2017, 10, 1734; doi:10.3390/en10111734.
- [35].D. A. Cantero et al. Reaction engineering for process identification of supercritical water biomass refining. J. of Supercritical Fluids 96 (2015) 21-35.
- [36].S. E. Hosseini, M. A. Wahid. Hydrogen production from renewable and sustainable energy resources: promising green energy carrier for clean development. Renewable and Sustainable Energy Reviews 57 (2016) 850-866.
- [37].L. Guo et al. Supercritical water gasification research and development in China. J. of Supercritical Fluids 96 (2015) 144-150.